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Phase-error Correction by Single-phase Phase-Locked Loops based on Transfer Delay

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Context



PLLs are used everywhere in the grid by

- Energy producers for quantification
- Grid manager and energy distributors for reliability and security
- Special energy consumers for power conditioning.

Goal: Harmonics detection in a 3-phase voltage system

Constraint: limited computational resources

Adjustment: How can I reduce the number of calculations? Or maybe buy a faster processor?

Solution: Use a singlephase PLL instead of a 3-phase PLL.



- PLLs details
 - 3-phases Synchrone Reference Frame PLL dqPLL
 Single Phase delay PLL dPLL
- Proposed solutions
- Simulation performances
- Conclusions and perspectives



PLLs details

3-Phase SRF PLL - dqPLL



- Stability condition: $k_p > 0$ and $k_i > 0$
- Robustness depends on k_p and k_i
- Stable for all input signal disturbances

Delay PLL - dPLL



- Stability condition: $k_p > 0$ and $k_i > 0$
- As robust as dqPLL
- No phase-error at rated PLL frequency
- Oscillating U_d error when signal ang. Vel. ω deviates from rated ang. Vel. ω_{ff}
 - U_d error freq. nears the double of the input signal freq.
 - U_d error ampl : $U \cdot \frac{\pi}{4} \cdot \epsilon_{\omega}$; $\epsilon_{\omega} = \frac{\omega \omega_{ff}}{\omega_{ff}}$
 - →Oscillating phase angle error + steady offset

Proposed solutions

For the delay PLL $\begin{cases} U_{\alpha} = U \cos(\omega t) \\ U_{\beta} = U_{\alpha} \left(t - \frac{1}{4} T_{0} \right) = U \sin\left(\omega t - \frac{\pi}{2} \varepsilon_{\omega} \right) & \text{with } \varepsilon_{\omega} = \frac{\omega - \omega_{0}}{\omega_{0}} \end{cases}$

$$\rightarrow U_d = U(-\Delta\theta + \alpha) + U\alpha \cos(2\theta - \Delta\theta - \alpha)$$
With $\alpha = \frac{\pi}{4} \cdot \epsilon_{\omega}$ (ϵ_{ω} as the relative frequency variation)

Non-oscillatory part: $U_{d0} = -U\Delta\theta + U\alpha$, Standardly controlled value

 $-U\Delta\theta + U\alpha = 0 \rightarrow \Delta\theta = \alpha \rightarrow \text{Steady phase angle offset}$

Phase angle error cancellation strategies

- Change the PI controller set-point to Uα
- Correct the final output phase position by α
- Correct the estimated U_{β} value obtained after the sample delay

The real relative angular velocity is unknown but is estimated just like the estimated delivered angular velocity



Proposed solutions

Solution 1: Change the PI controller set-point to $U\alpha$: dPLL-Csp



U is approximated to Uq

Solution 2: Correct the final output phase position by α : dPLL-Ca





Proposed solution

Solution 3: Corrected voltage β-component : dPLL-CUb

$$U_{\beta} = U \sin\left(\omega t - \frac{\pi}{2} \varepsilon_{\omega}\right) = U \sin(\omega t) \cos\left(\frac{\pi}{2} \varepsilon_{\omega}\right) - U_{\alpha} \sin\left(\frac{\pi}{2} \varepsilon_{\omega}\right)$$

Corrected β -component:

$$U_{\beta c} = \frac{U_{\beta} + U_{\alpha} \sin\left(\frac{\pi}{2} \,\widehat{\varepsilon_{\omega}}\right)}{\cos\left(\frac{\pi}{2} \,\widehat{\varepsilon_{\omega}}\right)}$$





Performances

Simulation configuration

- Matlab Simulink
- 20 kHz sample frequency
- 50 Hz input signal with an amplitude of 100
- Input signal disturbances: 20% amplitude increase at 0.3 sec, 15° phase angle jump at 0.4 sec and a 2% frequency increase at 0.7 sec

Phase-error after frequency change



Performances

PLLs Peak phase error in function of 5th harmonic amplitude



Filtered PLLs Peak phase error in function of 5th harmonic amplitude



Conclusion

- For single-phase PLL, the output phase-angle value oscillates with a constant offset error when the input signal frequency deviates from the PLL's rated frequency.
 - Frequency: very close to the double of that of the input frequency.
 - Constant offset value: proportional to the relative frequency variation
 - Amplitude: proportional to the input signal amplitude and the relative frequency variation.
- The three improvement approaches have good performances
 - The curative methods: cancel constant offset error
 - The preventive method: cancels offset + oscillations
- The proposed structures remain stable in harmonics presence
- Bandstop filters can be used
 since the oscillations frequency is known



Thanks



